

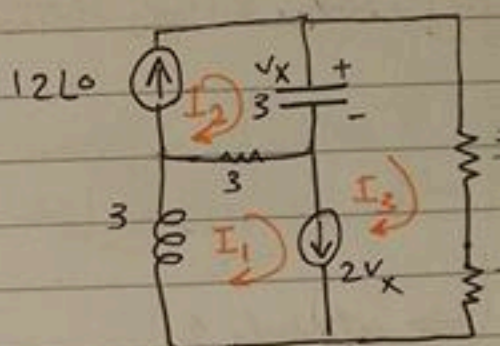
$$L = b - n + 1$$

$$6 - 4 + 1 = 3$$

ex:-1 independent  $\frac{L}{3}$  lines

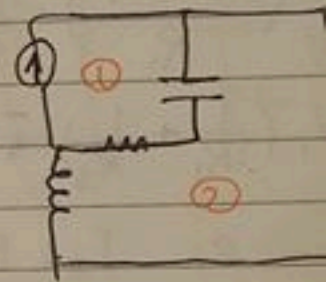
$$I_3 = 12 L_0$$

$$\Rightarrow 2V_X = I_1 - I_2$$



loop 1  $\Rightarrow 2(3 L_0 (I_3 - I_2)) = I_1 - I_2 \rightarrow \textcircled{1}$

$$\Rightarrow (3 + \frac{3L_0}{3})I_1 + (6 - \frac{3L_0}{3})I_2 - (3 - \frac{3L_0}{3})I_3 = 0$$



بالاعتماد بـ  $I_3$  في المعادلة 1

$$\therefore 6 L_0 (12 L_0 - I_2) = I_1 - I_2$$

$$\therefore I_1 + (6 L_0 - 1)I_2 = 72 L_0 \rightarrow *$$

$$\therefore (3 + \frac{3L_0}{3})I_1 + (\frac{6}{3} + \frac{3L_0}{3})I_2 = (\frac{3}{3} + \frac{3L_0}{3})12 L_0$$

$$\therefore (1 + L_0)I_1 + (2 + L_0)I_2 = 12 L_0 + 12 L_0$$

حل المعادلتين  $I_1 = \checkmark$   $I_2 = \checkmark$  \* \* \*



# [4] Node Voltage Method (Nodal Method)

طريقة العقد

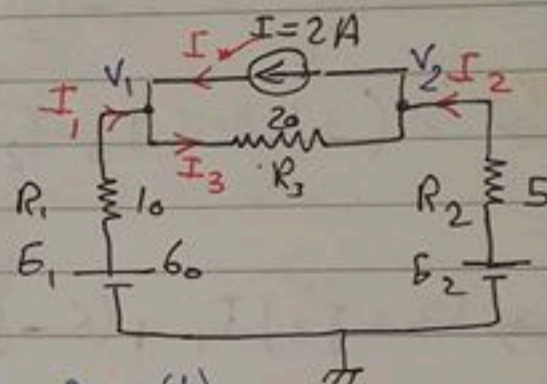
نحدد عدد Nodes التي في الدائرة ونسميها Node 1 و Node 2  
منهم Reference و نسميها "نوعها الأرضي".

⇒ at Node 1

$$I_1 + I = I_3$$

$$\left( \frac{E_1 - V_1}{R_1} \right) + 2 = \frac{V_1 - V_2}{R_3}$$

$$V_1 \left( \frac{1}{R_1} + \frac{1}{R_3} \right) - V_2 \left( \frac{1}{R_3} \right) = 2 + \frac{E_1}{R_1} \rightarrow (1)$$



Node 2:  $I_2 + I_3 = I \quad \therefore \frac{E_2 - V_2}{R_2} + \frac{V_1 - V_2}{R_3} = I$

$$-\frac{1}{R_3} V_1 + \left( \frac{1}{R_2} + \frac{1}{R_3} \right) V_2 = \frac{E_2}{R_2} - I \rightarrow (2)$$

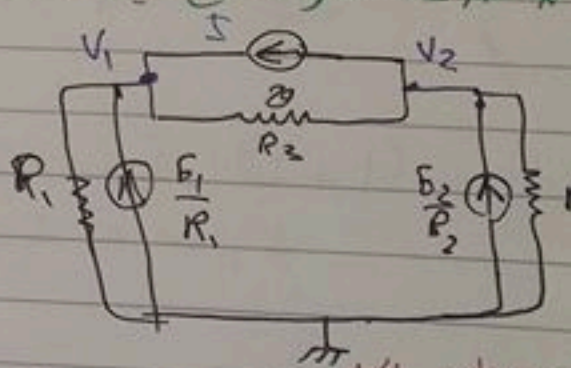
Format Methode.

\* طريقة أخرى أسرع في الحل

Node 1:  $V_1 \left( \frac{1}{R_1} + \frac{1}{R_3} \right) - \frac{1}{R_3} V_2 = \frac{E_1}{R_1} + I$

↓  
المطلوب هو مجموع ال Currents  
التي داخل - التي خارج

Node 2:  $-\frac{1}{R_3} V_1 + \left( \frac{1}{R_2} + \frac{1}{R_3} \right) V_2 = \frac{E_2}{R_2} - I$



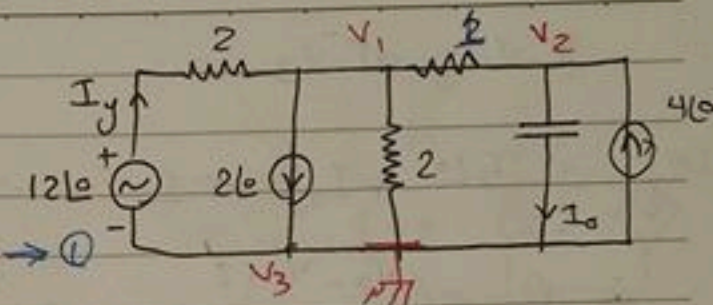
ترجع طريق الحل 1 -  
نحن نأخذ مثلا على Node 2

← معادل  $V_2$  = مجموع مقابلات القارمات التي داخله Node 2  
← معادل  $V_1$  = مقابلات القارمات التي خارج Node 1  
← والمطلوب = مجموع Current Sources التي داخل - التي خارج



Node 1

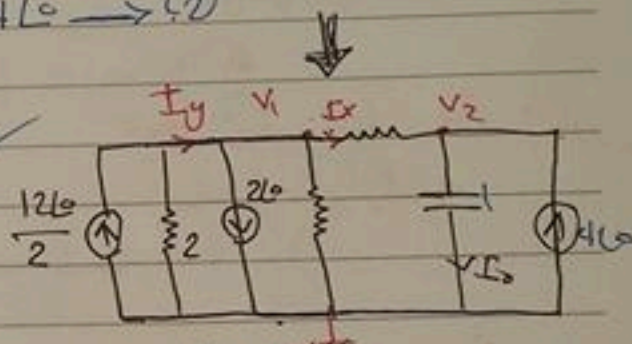
$$V_1 \left( \frac{1}{2} + \frac{1}{2} + 1 \right) - V_2(1) = 6 \angle 0 - 2 \angle 0 \rightarrow (1)$$



Node 2  $(V_2) \left( 1 - \frac{1}{j1} \right) - V_1(1) = 4 \angle 0 \rightarrow (2)$

$$\frac{I}{X} = \frac{V_1 - V_2}{1}$$

From 1, 2  $V_1, V_2$



$$I_o = \frac{V_2}{-j1}$$

From Circuit 1  $\rightarrow I_y = \frac{12 \angle 0 - V_1}{2}$

Power  $P_{1\Omega} \leftarrow$  voltage element of 5

$$\Rightarrow V_3 = 50 \angle 30$$

Node 1  $V_1 \left( \frac{1}{6-j8} + \frac{1}{-j5} \right)$

$$-V_2 \left( \frac{1}{6-j8} \right) = -5 \angle 0 \Rightarrow (1)$$

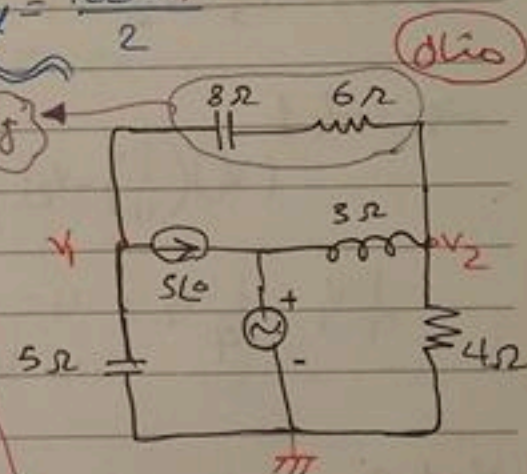
Node 2  $-V_1 \left( \frac{1}{6-j8} \right) + \left( \frac{1}{4} + \frac{1}{3} + \frac{1}{6-j8} \right) V_2$

$$-V_3 \left( \frac{1}{j3} \right) = 0 \Rightarrow (2)$$

$V_3 \angle V_2$  (0) 5 (1) mo

$$\Rightarrow P_{V.S} = 50 \times I_{V.S} \cos(30 - \theta_{I.V.S})$$

$$\Rightarrow I_1 = \frac{V_3 - V_2}{j3} = \checkmark$$



ملاحظة: لا يتم الimpedance  
تكون التوازي مع  
عنصرها المكافئ متوصل  
توازي مع المقاومة 6  
فيجب ملاحظة



K.V.L at  $V_3$

$$\therefore 5L + I_{V_3} = I_1 \quad \rightarrow I_{V_3} = L$$

$$\rightarrow P_{dis} = \left( \frac{V_2 - V_1}{6 - j8} \right)^2 \times 6 + \frac{V_2^2}{4}$$

↓

قوة مستقيمة زائدة لأن الباور  
مفيدة مستقيمة

$$P_{dis} = P_{vs} \quad \text{||}$$

$$\rightarrow V_3 - V_2 = 12 \rightarrow \textcircled{1}$$

⇒ Node 1

$$(V_1) \left( \frac{1}{4} \right) - V_2 \left( \frac{1}{4} \right) - V_3 \left( \frac{1}{8} \right) = 2 - 6$$

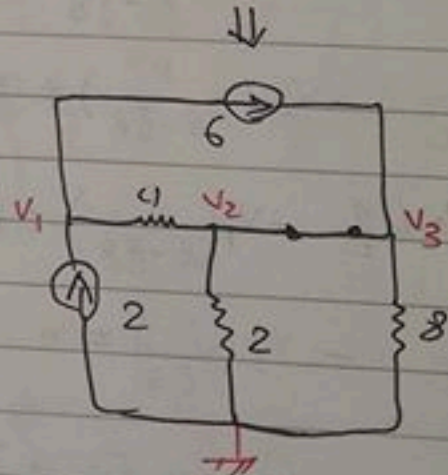
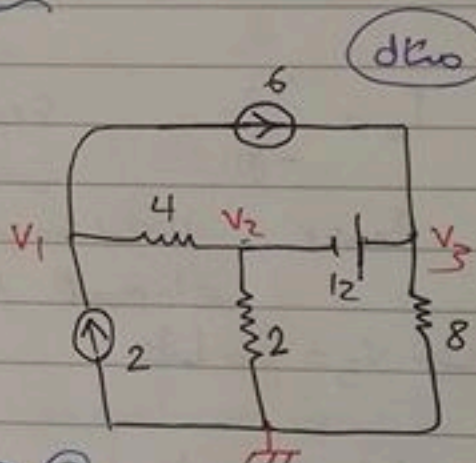
$$\therefore \frac{1}{4} V_1 - \frac{1}{4} V_2 + 4 = 0$$

$$\therefore V_1 - V_2 + 16 = 0 \rightarrow \textcircled{2}$$

Node 2

$$V_2 \left( \frac{1}{4} + \frac{1}{2} \right) - V_1 \left( \frac{1}{4} \right) - V_3 \left( \frac{1}{8} \right) = 6$$

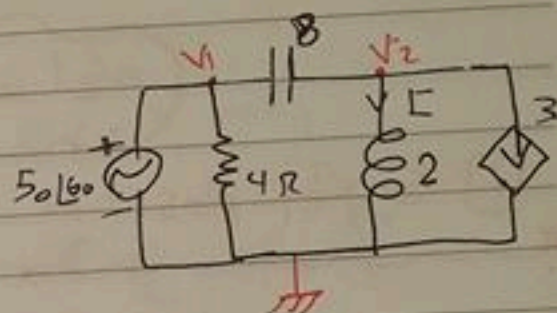
أو حل بـ 'loop analysis'  
هناك تيار في loop 3 بين الآتي تيار (1) معلوم



\*

$$V_1 = 50 \angle 60^\circ$$

Node 1  $\Rightarrow V_2$



$$V_2 \left( \frac{1}{j2} + \frac{1}{-j8} \right) - V_1 \left( \frac{1}{-j8} \right) = -3 \angle 0^\circ = \frac{V_2}{j2}$$

$$\therefore V_2 \left( \frac{1}{j2} + \frac{1}{-j8} \right) - \underset{50\sqrt{60}}{V_1 \left( \frac{1}{-j8} \right)} = -3 \frac{V_2}{j2}$$

$V_2 = \checkmark$  ← معادلة فيتي مجزول وللم



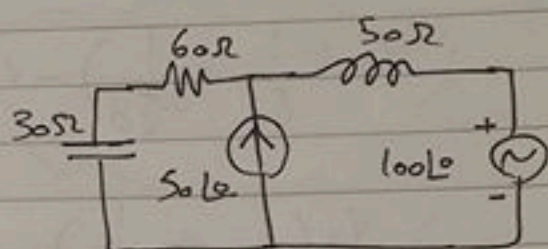
## Network theorem

## 1. Superposition

→ كل البايروستاتس المرتبطة  
independent sources =

ex: 1  $P_{60\Omega} = ?$ 

Solution

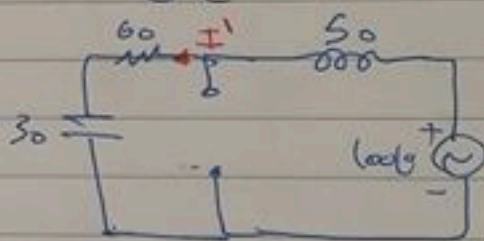


بشكل البايروستاتس مع كل البايروستاتس

## 1. Using V.S

Current source is ideal  $\rightarrow R = \infty$   
O.C

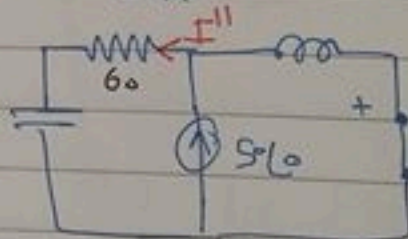
$$I' = \frac{100 \angle 0}{60 + j(50 - 30)} = \checkmark$$



## 2. Using C.S

Voltage source is ideal  $\rightarrow R = 0 \rightarrow S.R$

$$I'' = 5 \angle 0 \frac{50 \angle 90}{60 + j(50 - 30)} = \checkmark$$



$$\rightarrow I = I' + I'' = 3.953 \angle 71.5^\circ \text{ A}$$

$$P_{60\Omega} = (3.953)^2 \times 60 = \checkmark$$



$$P_{60} \neq P_1' + P_2''$$

ملحوظة ←

$$\Rightarrow P_1'' + P_2'' = I'^2 R + I''^2 R = R(I'^2 + I''^2)$$

$$\Rightarrow P_{60} = (I' + I'')^2 \times R \quad \therefore P_{60} \neq P_1' + P_2''$$

سؤال ممكن يتسأل في السطوي : \* الـ Power في Superposition  
بشيء ازاى ؟!!!!

① بتجيب الغير الخارفي الدائرة مرتين

\* مرة دال Current source ideal open circuit

\* ومرة دال Voltage source ideal short circuit

② جمع التيارات ونجيب التيار الكاف في ونزعه ونجيب نظره في المقاومة

(ملحوظة) في خاطة الكل بيقع فينا . غلط ، اننا نجيب الباور لكل دائرة ونجوعهم لأخر

$$P_{60} \neq P_1' + P_2''$$

مثال

\* using  $g_0$  Volt

by loop analysis :-

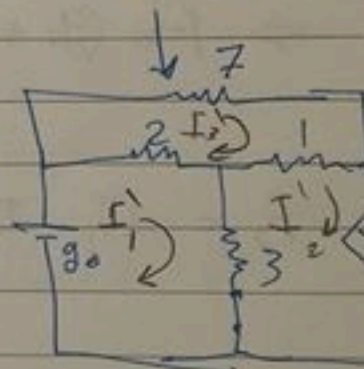
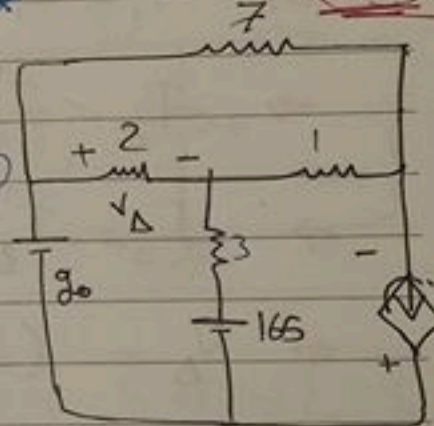
$$\text{loop 1} : (2+3)I_1' - (3)I_2' - 2I_3' = g_0 \rightarrow ①$$

$$\text{loop 2} : I_2' = 0.5 V_{\Delta} = 0.5 * (I_1' - I_3') \times 2$$

$$\therefore I_2' = I_1' - I_3' \rightarrow ②$$

$$\text{loop 3} : -2I_1' - I_2' + 10I_3' = 0 \rightarrow ③$$

$$I_3' \leq I_2' \leq I_1' \text{ بين ③ و ② و ①}$$



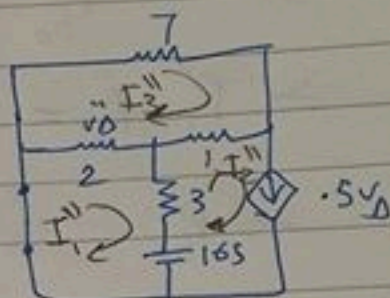


دکتر ابرار

\* using 165 volt

loop 1:-

$$(2+3)I_1'' - 3I_2'' - 2I_3'' = 165 \rightarrow (1)$$



loop 2:-

$$I_2'' = 0.5 V_{\Delta} = 0.5 (I_1'' - I_3'') \times 2$$

$$\therefore I_2'' = I_1'' - I_3'' \rightarrow (2)$$

loop 3:-  $10 I_3'' - 2 I_1'' - I_2'' = 0 \rightarrow (3)$

$$I_3'' \leq I_2'' \leq I_1'' \quad \text{من ۲ تا ۱ به ترتیب}$$

$$\Rightarrow I_1 = I_1' + I_1''$$

$$\Rightarrow I_2 = I_2' + I_2''$$

$$\Rightarrow I_3 = I_3' + I_3''$$

$$\Rightarrow V_{\Delta} = (I_1 - I_3) \times 2$$

$$\Rightarrow P = (g_0 \times I_1) + 165(I_1 - I_2) + \frac{1}{2} V_{\Delta} \times V_S$$

$$V_S = 7I_3 - g_0$$

روش K.V.L در هر یک از شاخه ها

$$P_{3\Omega} = (I_1 - I_2)^2 \times 3$$



ملحوظة بنسبهم ال Super position اجبالا اري لما يعني عندنا  
توجد حالت مختلفة

ex:-

اوجه ال  $15 V_c$

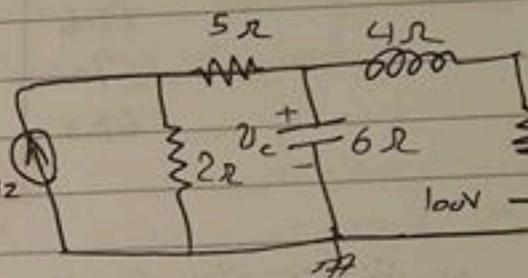
«مأخوذة اما يظن ان لا تكون المأخذ

يعني عايز ما دالة في الزمر  $V(t)$

$\rho = \text{independent}$  \*  $f = 50 \text{ Hz}$

حالا می

{ solution }

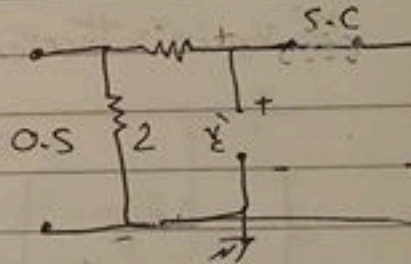


$\therefore$  Frequency  $\omega = \omega_0 \therefore \Rightarrow$  using super position.

① → using DC source :-

Current Source ideal.

$$\Rightarrow V_c = 100 \times \frac{7}{7+3} = 70 \text{ V}$$



② using a.c source

Voltage Source ideal

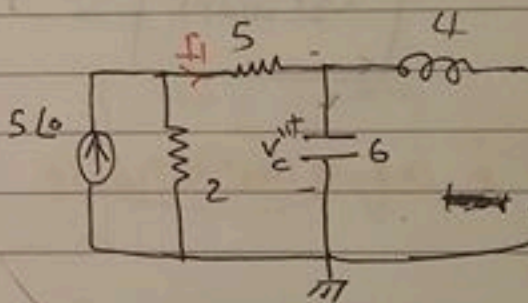
$$z_1 = (3 + j4) // (-j6)$$

$$z_2 = (5 + z_1)$$

$$I_1 = 5 \angle 0 \frac{2}{Z_2 + 2} \Rightarrow V_C = I_1 \cdot Z_2 = 5.433 \angle -1.10$$

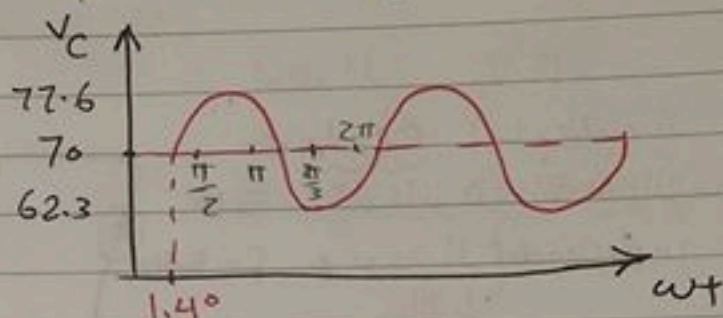
$$v_c'' = 5.4\sqrt{2} \sin(\omega t - 1.4)$$

المطلوب  $\Rightarrow v_c = v_c' + v_c'' = 70 + 5.4\sqrt{2} \sin(\omega t - 1.4)$



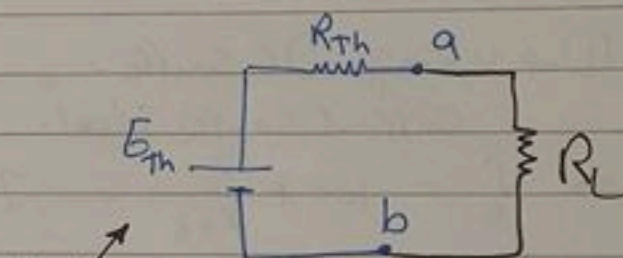
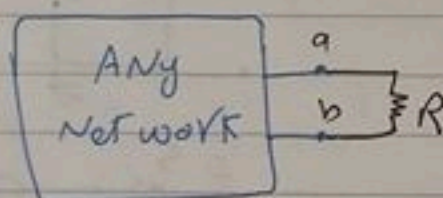


$$V_c = 70 + 7.6 \sin(\omega t - 1.4)$$



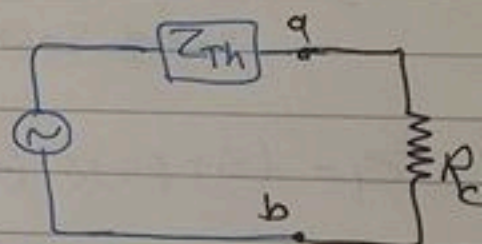
### \* Network theorem

Thevenin's Theorem :-



$\Delta$

$\Delta$



\* Original Network

\* Thevenin Equivalent Circuit

thevenin equi.  $\Delta$  Network  $\Delta$  Load

الطريقة الأولى

1. نفتح بين النقطتين a و b في الشبكة الأصلية

2. نحسب  $E_{oc}$  و  $E_{th}$  و  $E_{oc} = E_{th}$

3. نحسب بين النقطتين

4. نحسب  $I_{sc}$  و  $I_{th}$  و  $I_{sc} = I_{th}$

5. نحصل على Thevenin equivalent circuit

الطريقة الثانية



← الطريقة الثانية:

① Passive circuit الدائرة الجي

Passive curCuit :- یعنی نشیں کی CS independent و VC independent و CS independent و VC independent

ونشيل كل  $v \in \text{independent}$  ونظ مكانه  $\underline{\text{S.C}}$   
ونفتح بين المقطعين  $a, b$  ونصلهم بالدائرة عند بين المقطعين  
بين  $R_{th}$  هي  $R_{th}$

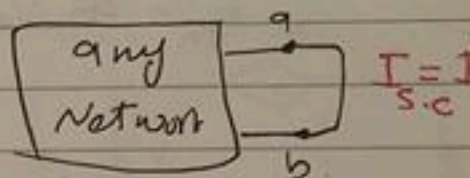
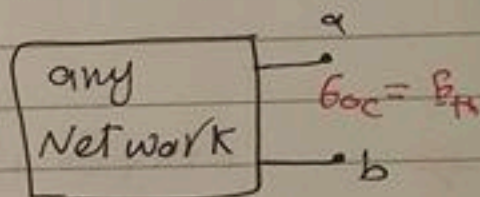
$R_{th} = \frac{E_g}{I_g}$

thevenin equivalent circuit for  $j\omega$  (4)

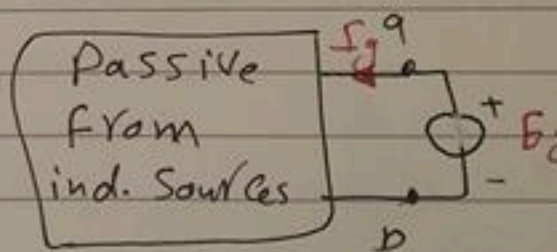
$$G_{o.c} = G_{TH}$$

$$I_{S.C} = I_{th}$$

$$\therefore R_{th} = \frac{E_{oc}}{I_{sc}}$$



$$R_{th} = \frac{E_g}{I_g}$$



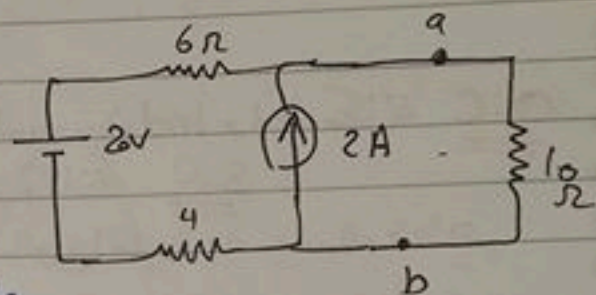
Passive <sup>id</sup>Circuit  $\rightarrow$  ind. V.S  $\rightarrow$  S.C  
                   $\searrow$  ind C.S  $\rightarrow$  O.C

والـ *dependant* بفعل في الدائرة عادي.



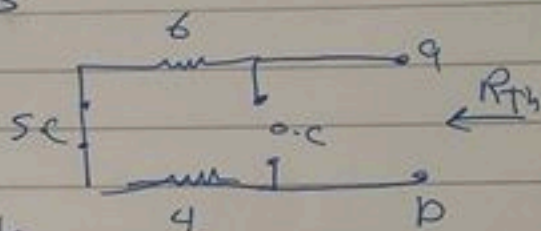
ex:-

Solution



عشانه جيب  $R_{th}$  منقول الدايه Passive  
يعز مقيس اى معار للجهد او التيار  
كله مقاومات او Impedance

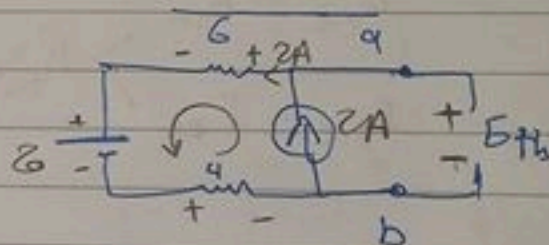
$$\Rightarrow \therefore R_{th} = 6 + 4 = 10 \Omega$$



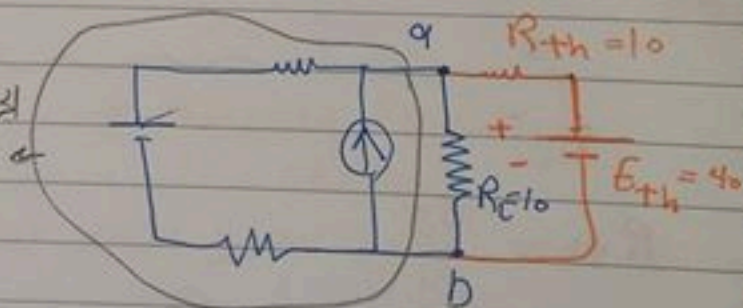
عشانه جيب ال  $E_{th}$  منقول ac على الدايه

$$\Rightarrow -E_{th} + 20 + ((4+6) \times 2) = 0$$

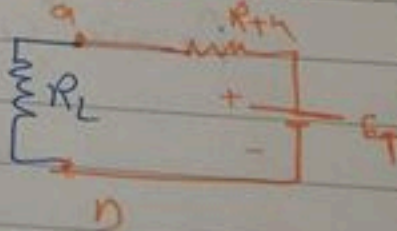
$$\therefore E_{th} = 40 \text{ Volt}$$



لتردد كلة نشيلا



Thevenin Equivalent

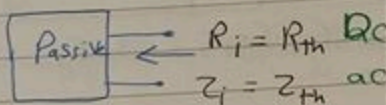




$R_{th}$ ,  $Z_{th}$

independent source

$$R_{th} = R_i$$

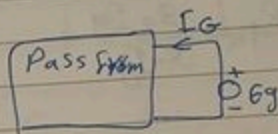


$$R_{th} = \frac{E_{oc}}{I_{oc}}$$

$$Z_{th} = \frac{E_{oc}}{I_{sc}}$$

$$(1) R_{th} = \frac{E_{oc}}{I_{sc}} \quad dc$$

$$(2) Z_{th} = \frac{E_{oc}}{I_{sc}} \quad ac$$

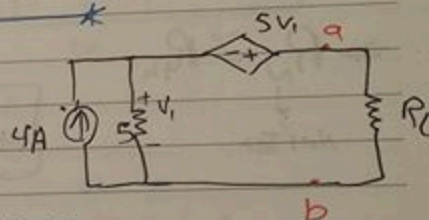


$$R_{th} = \frac{E_g}{I_g}$$

$$Z_{th} = \frac{E_g}{I_g}$$

$$E_{th} = E_{ac}$$

$\rightarrow$  K.V.L  $V_1 + 5V_1 - E_{th} = 0$   
 $E_{th} = 6V_1 = 6(5 \times 4) = 120V$



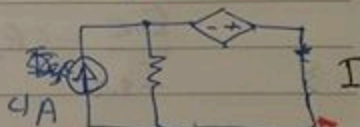
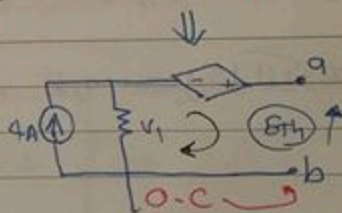
Ex 11  
 11/10/20  
 ①  $R_{th}$   $R_{th} = \frac{E_{oc}}{I_{sc}} = \frac{120}{10}$

$\rightarrow$  K.V.L  $\rightarrow 6V_1 = 0 \rightarrow V_1 = 0$

$\rightarrow$  K.C.L  $4 = -I_{sc} + \frac{V_1}{5}$

$\rightarrow I_{sc} = 4$

$\therefore R_{th} = \frac{120}{4} = 30$

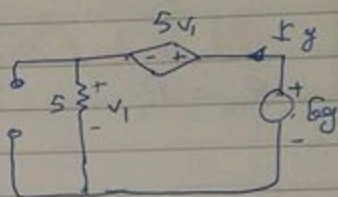


Hi. Star  
 S.E



المقاومة المستقلة  $I_s$   $\rightarrow$  independent  
 Current Source  $\rightarrow$  O.C  
 Voltage Source  $\rightarrow$  S.C

$$R_{th} = \frac{E_g}{I_g}$$



$\rightarrow$  K.V.L  
 $\therefore V_1 + 5V_1 - E_g = 0$

$$E_g = 5V_1 + V_1 = 6V_1 \quad \text{and} \quad I_g = 5V_1 \Rightarrow 6 \times I_g \times 5 = 30 I_g$$

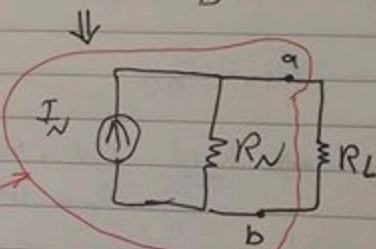
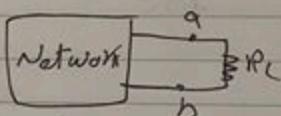
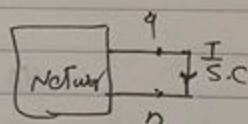
$$\therefore R_{th} = \frac{30 I_g}{I_g} = 30$$

$\Rightarrow$  Norton theorem:-

$$\Rightarrow I_N = I_{s.c}$$

$$\Rightarrow R_N = R_{th}$$

Norton



Norton equivalent.

\* لنصل بين مكافئ نورتن بين نقطتي a, b لنصل كل المكونة  
 الى عدد بين النقطتين a, b لنصل بين a و b  
 ① S.C ونجيب  $I_{s.c}$   
 ② O.C ونجيب  $E_{o.c}$

$$\frac{E_{o.c}}{I_{s.c}} = R_{th} = R_N$$



40 اهمي ٤٥ وولٽي ذريعو ٽيڪٽيڪل ٿيڻ

$$I_N = I_{S.C}$$

⇒ loop analysis

$$\text{loop 1} \Rightarrow (5 + 30 + 20)I_1 - 50I_{S.C} = 100 \rightarrow (1)$$

$$\text{loop 2} \Rightarrow -50I_1 + 100I_{S.C} = -100 \rightarrow (2)$$

$$-4I_1 + 100I_{S.C} = 0 \rightarrow (2)$$

ٽيڪٽيڪل ٿيڻ

$$I_{S.C} = I_N$$

$$I_{S.C} = \frac{1}{2} \rightarrow I_N$$

$$\therefore R_N = R_{Th} = \frac{E_{oc}}{I_{S.C}} = \frac{60.5}{1/2} = 121 \Omega$$

at o.c. →

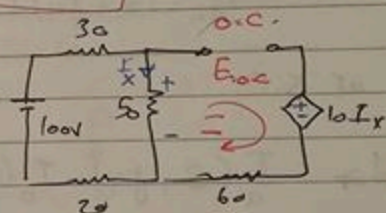
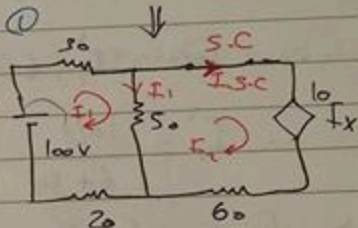
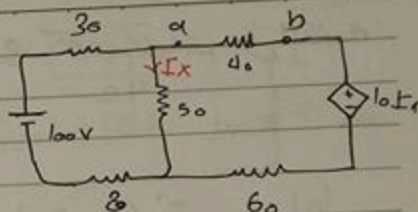
KVL

$$50I_x - 60 - 10I_x = 0$$

$$\Rightarrow I_x = 100/100 = 1A$$

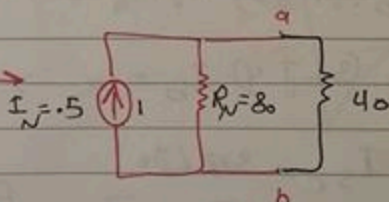
$$\therefore E_{oc} = 40 \text{ V}$$

$$\therefore R_N = \frac{40}{1/2} = 80 \Omega$$



ٽيڪٽيڪل ٿيڻ

اڳي ٿيڻ





Ex:-

المسألة هي نستخدم على القواعد

⇒ K.VL

$$10\angle 0 - I_1(3+j4) - 3I_1 = 0$$

$$\therefore 10\angle 0 - I_1(6+j4) = 0$$

$$\therefore I_1 = \frac{10\angle 0}{6+j4}$$

$$\Rightarrow E_{th} = 3I_1 + j4 * I_1$$

$$\therefore E_{th} = (3+j4)I_1 = \checkmark = 6.93 \angle 19.44$$

at S.C

$$\text{loop 1} \Rightarrow I_a(3+j4) - I_b(j4) = 10\angle 0 - 3I_a$$

$$\therefore (3+j4)I_a - j4I_b = 10\angle 0 - 3I_a$$

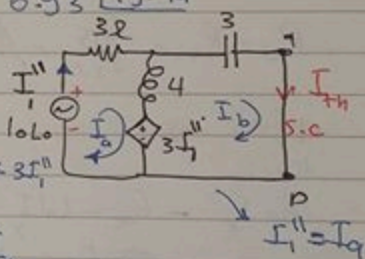
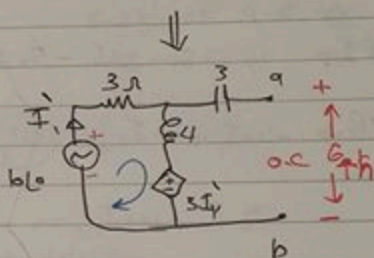
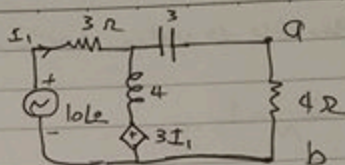
$$(6+j4)I_a - j4I_b = 10\angle 0 \rightarrow (1)$$

$$\text{loop 2} \Rightarrow I_b(j4-j3) - j4I_a = 3I_a = 3I_b$$

$$jI_a - (3-j4)I_b = 0 \rightarrow (2)$$

$$I_{S.C} = 3.33 \angle 0$$

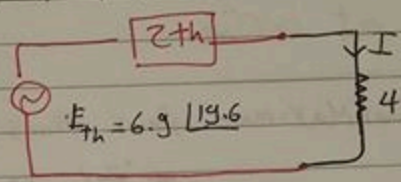
$$Z_{th} = Z_N = \frac{E_{o.c}}{I_{S.C}} = 2.08 \angle -70.56$$





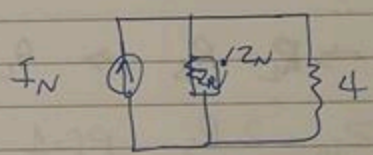
2020-70-86

⇒ مكافئ سلف  
للدائرة



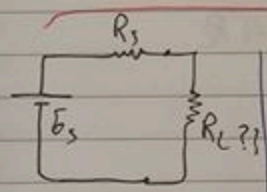
$$P = (1.36)^2 \times 4 \text{ watt}$$

لو طلبت مكافئ ثوريته لثقل نفس الخطوات بس امانيع بنرسم  
↓



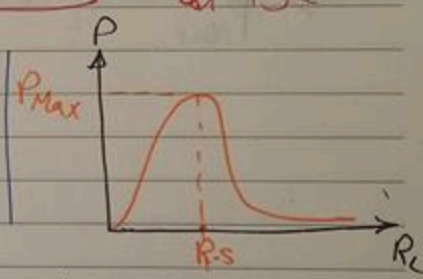
### \* Maximum Power Transfer Theorem

at DC



$$P_L = \left( \frac{E_s}{R_s + R_L} \right)^2 R_L$$

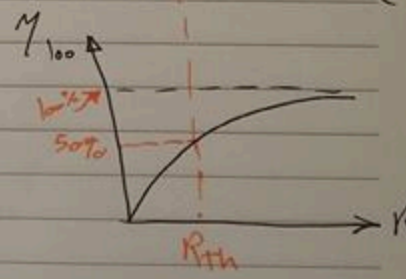
$$= \frac{E_s^2 R_L}{(R_s + R_L)^2}$$



$$\frac{\partial P_L}{\partial R_L} = 0$$

مشتق = 0 ⇒ R\_L = R\_s

$$P_{Max} = \frac{E_s^2}{4R_s}$$

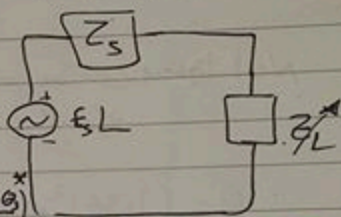




at ac  $\rightarrow$

For Maximum power transfer

$$Z_L = Z_S^* \rightarrow Z_S = (R_S + jX_S)^* = (Z_S \angle \theta_S)^*$$



معيار الزاوية  $\theta_S$   $\rightarrow$   $\theta_L = -\theta_S$

$$\therefore Z_L = Z_S \angle \theta_L \quad \theta_L = -\theta_S$$

$$\Rightarrow R_L = R_S \Rightarrow \theta_L = -\theta_S$$

$$\text{مثال} \Rightarrow Z_{in} = 2 R_S \quad \text{PF} = 1$$

$Z_{in} = Z_S + Z_L$

$$\begin{cases} Z_S = R_S \angle \theta_S \\ Z_L = R_S \angle \theta_L \end{cases}$$

$$\Rightarrow P_{Max} = I_L^2 * R_L = \left( \frac{E_S}{2R_L} \right)^2 R_L = \frac{E_S^2}{4R_L}$$